

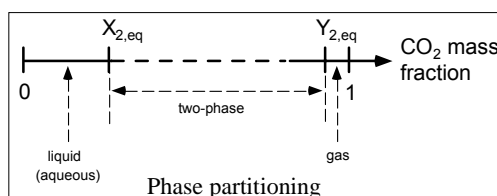
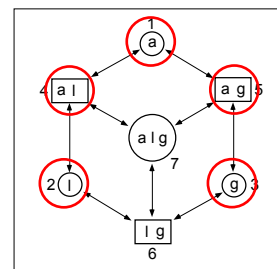
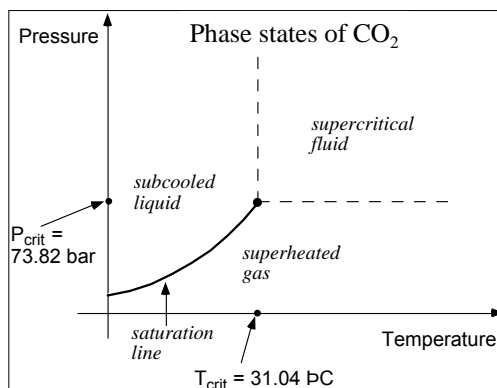


# Problem ECO2N: Radial Flow from a CO<sub>2</sub> Injection Well

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## ECO2N for Water-NaCl-CO<sub>2</sub>



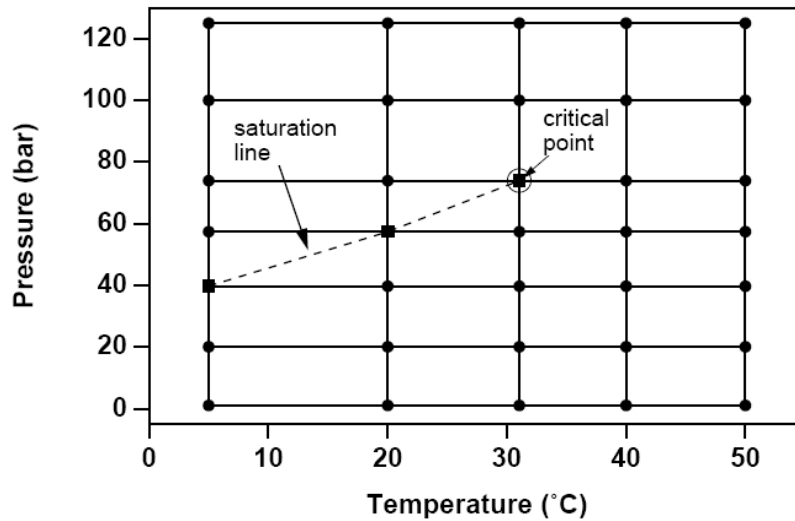
Possible phase combinations in the system water-CO<sub>2</sub>:

- a – aqueous
- l – liquid CO<sub>2</sub>
- g – gaseous CO<sub>2</sub>.

Separate liquid and gas phases exist only at subcritical conditions.

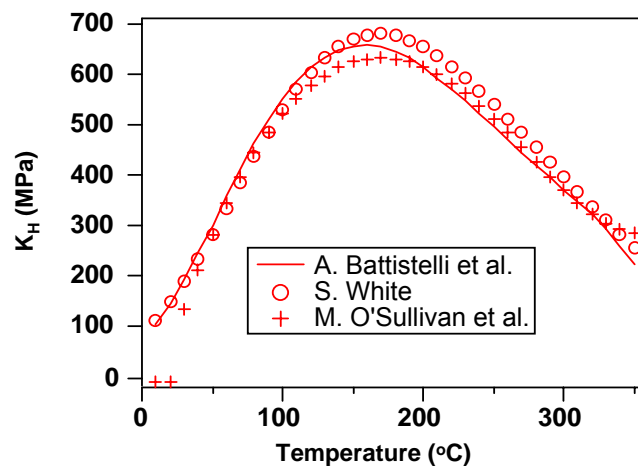
2

## Tabulation of CO<sub>2</sub> Properties



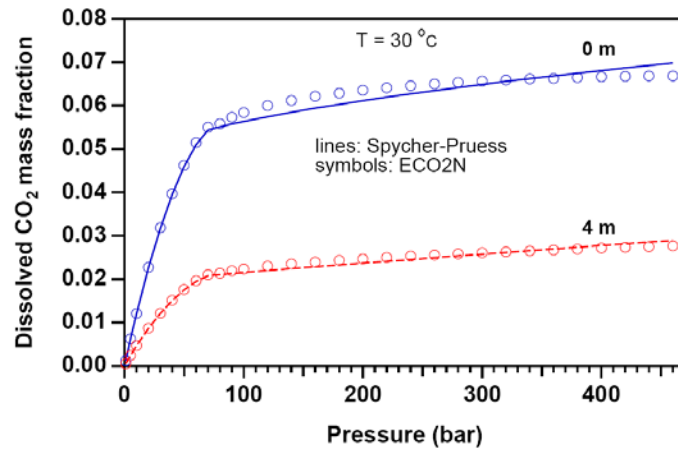
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## Henry's Coefficient for Dissolution of CO<sub>2</sub> in Liquid Water



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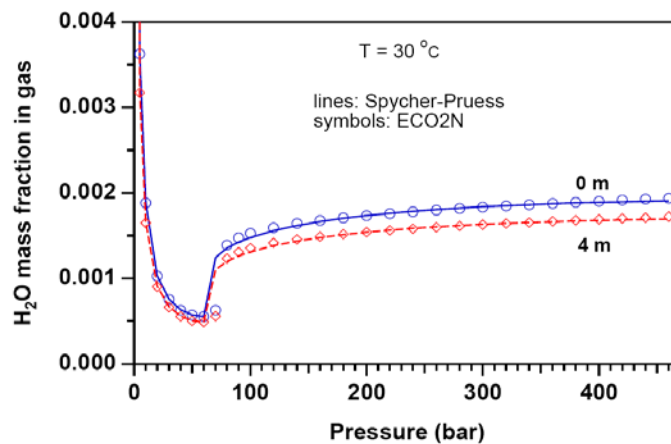
## Dissolution of CO<sub>2</sub> in Brine



Dissolved CO<sub>2</sub> mass fractions in two-phase system at T = 30 °C for pure water (0 m) and 4-molal NaCl brine. Lines represent the original correlation of Spycher and Pruess (2005) that uses a Redlich-Kwong EOS for molar volume of CO<sub>2</sub>. Symbols represent data calculated by ECO2N in which the molar volume of CO<sub>2</sub> is obtained from the correlations of Altunin (1975)

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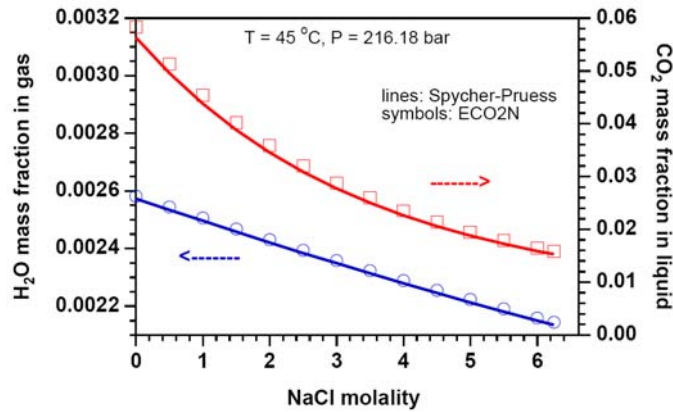
## H<sub>2</sub>O Mass Fraction in CO<sub>2</sub>-Rich Phase



H<sub>2</sub>O mass fractions in gas in two-phase system at T = 30 °C for pure water (0 m) and 4- molal NaCl brine. Lines represent the original correlation of Spycher and Pruess (2005) that uses a Redlich-Kwong EOS for molar volume of CO<sub>2</sub>. Symbols represent data calculated by ECO2N in which the molar volume of CO<sub>2</sub> is obtained from the correlations of Altunin (1975).

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## H<sub>2</sub>O Concentration in Gas, CO<sub>2</sub> Concentration in Brine



Concentration of water in gas and CO<sub>2</sub> in the liquid (aqueous) phase at (T, P) = (45 °C, 216.18 bar), for salinities ranging from zero to fully saturated. Lines were calculated from the correlation of Spycher and Pruess (2005) that uses a Redlich-Kwong EOS for molar volume of CO<sub>2</sub>. Symbols represent data calculated by ECO2N from a modified correlation in which the molar volume of CO<sub>2</sub> is obtained from the correlations of Altunin (1975).

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## Summary of ECO2N

<b>Components</b>	# 1: water # 2: NaCl # 3: CO <sub>2</sub>
<b>Parameter choices</b>	(NK, NEQ, NPH, NB) = (3, 4, 3, 6) water, NaCl, CO <sub>2</sub> , nonisothermal (default) (3, 3, 3, 6) water, NaCl, CO <sub>2</sub> , isothermal molecular diffusion can be modeled by setting NB = 8
<b>Primary Variables</b>	<p>single fluid phase (only aqueous, or only gas)<sup>#</sup> (P, X<sub>sm</sub>, X3, T)</p> <p>P - pressure X<sub>sm</sub> - salt mass fraction X<sub>s</sub> in two-component water-salt system, or solid saturation S<sub>s</sub>+10 X3 - CO<sub>2</sub> mass fraction in the aqueous phase, or in the gas phase, in the three-component system water-salt-CO<sub>2</sub> T - temperature</p> <p>two fluid phases (aqueous and gas)<sup>#</sup> (P, X<sub>sm</sub>, S<sub>g</sub>+10, T)</p> <p>P - pressure X<sub>s</sub> - salt mass fraction X<sub>s</sub> in two-component water-salt system, or solid saturation S<sub>s</sub>+10 S<sub>g</sub> - gas phase saturation T - temperature</p>
# in addition there may be solid salt	

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## SELEC Block for ECO2N (1 of 2)

- Dependence of *permeability* on the fraction  $\phi_f$   $\phi_0 = (1-S_s)$  of original pore space that remains available to fluids:
  - 0: permeability does not vary with  $\phi_f$
  - 1:  $k = k_0 = (1-S_s)^{\gamma}$
  - 2: fractures in series
  - 3: tubes-in-series
- Model for *water solubility* in  $\text{CO}_2$ :
  - 0: after Spycher and Pruess (2005)
  - 1: evaporation model; i.e., water density in the  $\text{CO}_2$ -rich phase is calculated as density of saturated water vapor at prevailing temperature and salinity
- Dependence of *brine density* on dissolved  $\text{CO}_2$ :
  - 0: brine density varies with dissolved  $\text{CO}_2$  concentration according to García (2001)
  - 1: brine density is independent of  $\text{CO}_2$  concentration

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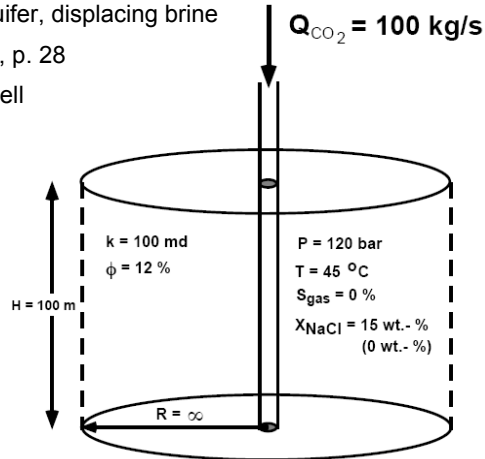
## SELEC Block for ECO2N (2 of 2)

- Thermophysical properties as a function of *salinity*
  - 0: full dependence.
  - 1: no salinity dependence of thermophysical properties (except for brine enthalpy; salt solubility constraints are maintained).
- Correlation for *brine enthalpy* at saturated vapor pressure
  - 0: after Lorenz et al. (2000).
  - 1: after Michaelides (1981).
  - 2: after Miller (1978).
- PVT properties of  $\text{CO}_2$  on file **CO2TAB**

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# Radial Flow from a CO<sub>2</sub> Injection Well

- CO<sub>2</sub> injection into saline aquifer, displacing brine
- ECO2N manual Section 5.2, p. 28
- Sample2\_CO2\_Injection\_Well
- Input file gcc3



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## MESH Generation: Radial Flow

```
*rcc3* ... Code Intercomparison problem3: Radial flow from a CO2 Injection Well
MESHMAKER1-----2-----3-----4-----5-----6-----7-----8
RZ2D
RADII
1
0.
EQUID
1
LOGAR
200
LOGAR
100
LOGAR
100
LOGAR
34
LAYER-----1-----2-----3-----4-----5-----6-----7-----8
1
100.
ENDFI-----1-----2-----3-----4-----5-----6-----7-----8
```

```
ELEME --- 435 1 1 434 .00000100000.000
A1 1 2 .2827E+02 .5655E+00 .3000E+00 -.5000E+02
A1 2 1 .8728E+02 .1746E+01 .4532E+00 -.5000E+02
A1 3 1 .1501E+03 .3002E+01 .7630E+00 -.5000E+02
A1 4 1 .2169E+03 .4339E+01 .1079E+01 -.5000E+02
...
...
CONNE
A1 1A1 2 1 .1500E-05 .1532E+00 .1885E+03
A1 2A1 3 1 .1532E+00 .1565E+00 .3811E+03
A1 3A1 4 1 .1565E+00 .1599E+00 .5778E+03
...
```

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## Input File for Radial Flow Problem

```
*rcc3* ... Code Intercomparison problem3: Radial flow from a CO2 Injection Well
ROCKS-----1-----2-----3-----4-----5-----6-----7-----8
SAND 2 2600.e00 .12 100.e-15 100.e-15 100.e-15 2.51 920.
4.5e-10
7 .457 .30 1. .05
7 .457 .00 5.1e-5 1.e7 .999
well 2 2600.e40 .12 100.e-15 100.e-15 100.e-15 2.51 920.
4.5e-10
7 .457 .30 1. .05
7 .457 .00 5.1e-5 1.e7 .999

MULTI-----1-----2-----3-----4-----5-----6-----7-----8
3 3 3 6
SELEC.....2.....3.....4.....5.....6.....7.....8.....9.....10.....11.....12.....13.....14.....15.....16
1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
.8 .8
SOLVR-----1-----2-----3-----4-----5-----6-----7-----8
5 Z1 00 8.0e-1 1.0e-7
START-----1-----2-----3-----4-----5-----6-----7-----8
-----1 MOP: 123456789*123456789*1234 -----5-----6-----7-----8
PARAM-----1-----2-----3-----4-----5-----6-----7-----8
1 999 9991000300000000 4 3
8.64e8 -1.
1.
1.E-5 1.E00
120.e5 .15 0.0 45.
FOFT -----1-----2-----3-----4-----5-----6-----7-----8
A1 49 1 .1745E+04 .2685E+03 .2570E+02 -.6500E+01
A12 2 1 .3080E+08 .4738E+07 .1080E+04 -.6500E+01

GENER-----1-----2-----3-----4-----5-----6-----7-----8
A1 linj 1 COM3 100.

INCON-----1-----2-----3-----4-----5-----6-----7-----8

TIMES-----1-----2-----3-----4-----5-----6-----7-----8
4
2.592E+06 8.64E+06 8.64E+07 8.64E+08
ENDCY-----1-----2-----3-----4-----5-----6-----7-----8
```

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## rcc3

- Generate radial mesh using MESHMAKER, RZ2D
- Edit mesh according to instructions in manual
- Look at input file rcc3 and answer the following questions prior to running the simulation:

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## Questions rcc3

- Is this an isothermal or non-isothermal simulation?  
\_\_\_\_\_
- What approximate overpressure is needed for CO<sub>2</sub> to displace brine? \_\_\_\_\_  
\_\_\_\_\_
- Fully describe the initial conditions in the saline aquifer: \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

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## Questions rcc3

- Run rcc3; answer the following questions:
- Describe the time-stepping and convergence behavior during the first few time steps: \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_
- Describe the system state after 100 years of CO<sub>2</sub> injection: \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

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# Output from Radial Flow Problem

```
...ITERATING... AT [ 1, 1] --- DELTEX = 0.100000E+01 MAX. RES. = 0.353732E+01 AT ELEMENT Al 1 EQUATION 3
$$$$$$$$$$$ GAS PHASE EVOLVES AT ELEMENT *Al 1* $$$$$$ X3 = 0.267978E-01 XCO2aq = 0.262048E-01 PX = 0.136627E+08 PA
...ITERATING... AT [ 1, 2] --- DELTEX = 0.100000E+01 MAX. RES. = 0.246617E-01 AT ELEMENT Al 2 EQUATION 3
$$$$$$$$$$$ GAS PHASE DISAPPEARS AT ELEMENT *Al 1* $$$$$$ SG = -.904072E-04
$$$$$$$$$$$ GAS PHASE EVOLVES AT ELEMENT *Al 1* $$$$$$ X3 = 0.262048E-01 XCO2aq = 0.261505E-01 PX = 0.135423E+08 PA
...ITERATING... AT [ 1, 3] --- DELTEX = 0.100000E+01 MAX. RES. = 0.123381E-01 AT ELEMENT Al 1 EQUATION 3
$$$$$$$$$$$ GAS PHASE DISAPPEARS AT ELEMENT *Al 1* $$$$$$ SG = -.100409E-03
...ITERATING... AT [ 1, 4] --- DELTEX = 0.100000E+01 MAX. RES. = 0.890409E-02 AT ELEMENT Al 1 EQUATION 3
...ITERATING... AT [ 1, 5] --- DELTEX = 0.100000E+01 MAX. RES. = 0.318444E-04 AT ELEMENT Al 1 EQUATION 3
Al 1( 1, 6) ST = 0.100000E+01 DT = 0.100000E+01 DX1= 0.166338E+07 DX2= -.220039E-15 T = 45.000 P = 13663377. S = 0.000000E+00
...ITERATING... AT [ 2, 1] --- DELTEX = 0.100000E+01 MAX. RES. = 0.100000E+01 AT ELEMENT Al 1 EQUATION 3
$$$$$$$$$$$ GAS PHASE EVOLVES AT ELEMENT *Al 1* $$$$$$ X3 = 0.515157E-01 XCO2aq = 0.264066E-01 PX = 0.141315E+08 PA
...ITERATING... AT [ 2, 2] --- DELTEX = 0.100000E+01 MAX. RES. = 0.986667E+00 AT ELEMENT Al 1 EQUATION 3
...ITERATING... AT [ 2, 3] --- DELTEX = 0.100000E+01 MAX. RES. = 0.906190E+00 AT ELEMENT Al 2 EQUATION 3
...ITERATING... AT [ 2, 4] --- DELTEX = 0.100000E+01 MAX. RES. = 0.171549E+00 AT ELEMENT Al 2 EQUATION 3
...ITERATING... AT [ 2, 5] --- DELTEX = 0.100000E+01 MAX. RES. = 0.110501E-01 AT ELEMENT Al 2 EQUATION 3
...ITERATING... AT [ 2, 6] --- DELTEX = 0.100000E+01 MAX. RES. = 0.115547E-03 AT ELEMENT Al 2 EQUATION 3
Al 2( 2, 7) ST = 0.200000E+01 DT = 0.100000E+01 DX1= 0.111159E+07 DX2= 0.974701E-07 T = 45.000 P = 14270651. S = 0.000000E+00
...ITERATING... AT [ 3, 1] --- DELTEX = 0.100000E+01 MAX. RES. = 0.496177E+00 AT ELEMENT Al 1 EQUATION 3
...ITERATING... AT [ 3, 2] --- DELTEX = 0.100000E+01 MAX. RES. = 0.124120E-01 AT ELEMENT Al 1 EQUATION 3
...ITERATING... AT [ 3, 3] --- DELTEX = 0.100000E+01 MAX. RES. = 0.252259E-04 AT ELEMENT Al 2 EQUATION 3
Al 1( 3, 4) ST = 0.300000E+01 DT = 0.100000E+01 DX1= 0.158370E+07 DX2= 0.972615E-05 T = 45.000 P = 17948923. S = 0.722178E-01
...ITERATING... AT [ 4, 1] --- DELTEX = 0.200000E+01 MAX. RES. = 0.661797E+00 AT ELEMENT Al 1 EQUATION 3
...ITERATING... AT [ 4, 2] --- DELTEX = 0.200000E+01 MAX. RES. = 0.745778E+00 AT ELEMENT Al 2 EQUATION 3
...ITERATING... AT [ 4, 3] --- DELTEX = 0.200000E+01 MAX. RES. = 0.679967E-01 AT ELEMENT Al 2 EQUATION 3
...ITERATING... AT [ 4, 4] --- DELTEX = 0.200000E+01 MAX. RES. = 0.594905E-03 AT ELEMENT Al 2 EQUATION 3
Al 2( 4, 5) ST = 0.500000E+01 DT = 0.200000E+01 DX1= 0.259505E+06 DX2= -.563856E-06 T = 45.000 P = 14951272. S = 0.000000E+00
...ITERATING... AT [ 5, 1] --- DELTEX = 0.200000E+01 MAX. RES. = 0.523482E+00 AT ELEMENT Al 2 EQUATION 3
...ITERATING... AT [ 5, 2] --- DELTEX = 0.200000E+01 MAX. RES. = 0.378805E+00 AT ELEMENT Al 2 EQUATION 3
...ITERATING... AT [ 5, 3] --- DELTEX = 0.200000E+01 MAX. RES. = 0.890199E-02 AT ELEMENT Al 2 EQUATION 3
Al 2( 5, 4) ST = 0.700000E+01 DT = 0.200000E+01 DX1= 0.957718E+05 DX2= -.261078E-05 T = 45.000 P = 15047044. S = 0.000000E+00
...ITERATING... AT [ 6, 1] --- DELTEX = 0.400000E+01 MAX. RES. = 0.132942E+01 AT ELEMENT Al 2 EQUATION 3
$$$$$$$$$$$ GAS PHASE EVOLVES AT ELEMENT *Al 2* $$$$$$ X3 = 0.414314E-01 XCO2aq = 0.267721E-01 PX = 0.150490E+08 PA
...ITERATING... AT [ 6, 2] --- DELTEX = 0.400000E+01 MAX. RES. = 0.103059E+01 AT ELEMENT Al 2 EQUATION 3
...ITERATING... AT [ 6, 3] --- DELTEX = 0.400000E+01 MAX. RES. = 0.896260E+00 AT ELEMENT Al 3 EQUATION 3
...ITERATING... AT [ 6, 4] --- DELTEX = 0.400000E+01 MAX. RES. = 0.219633E+00 AT ELEMENT Al 3 EQUATION 3
...ITERATING... AT [ 6, 5] --- DELTEX = 0.400000E+01 MAX. RES. = 0.164693E-01 AT ELEMENT Al 3 EQUATION 3
...ITERATING... AT [ 6, 6] --- DELTEX = 0.400000E+01 MAX. RES. = 0.150149E-03 AT ELEMENT Al 3 EQUATION 3
Al 3( 6, 7) ST = 0.110000E+02 DT = 0.400000E+01 DX1= 0.392177E+06 DX2= -.150040E-06 T = 45.000 P = 14761447. S = 0.000000E+00
```

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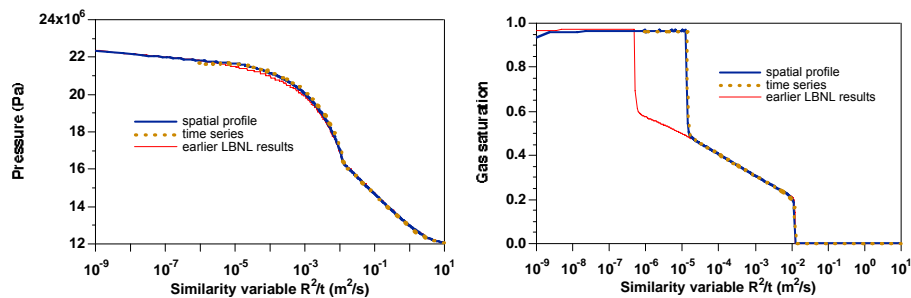
# Output from Radial Flow Problem

\*roc3\* ... Code Intercomparison problem3: Radial flow from a CO2 Injection Well

```
OUTPUT DATA AFTER ( 358, 5)-2-TIME STEPS THE TIME IS 0.100000E+04 DAYS
*****
TOTAL TIME KVCYC ITER ITERC KON DX1M DX2M DX3M MAX. RES. NER KER DELTEX
0.864000E+08 358 5 2476 2 0.14482E+06 0.68369E-01 0.11142E+00 0.85015E-06 59 2 0.14599E+07
*****
ELEM. INDEX P T SG SS XNACL YH2OG XCO2aq PCAP k-red. DG DL
(Pa) (deg-C) (kg/m3) (kg/m3)
Al 1 1 0.221350E+08 45.00 0.93159E+00 0.68408E-01 0.00000E+00 0.00000E+00 0.15977E-01 -.94561E+07 0.10000E+01 836.33 0.00
Al 2 2 0.22273E+08 45.00 0.95700E+00 0.42995E-01 0.00000E+00 0.00000E+00 0.15964E-01 -.94561E+07 0.10000E+01 835.64 0.00
Al 3 3 0.22197E+08 45.00 0.95823E+00 0.41769E-01 0.00000E+00 0.00000E+00 0.15952E-01 -.94561E+07 0.10000E+01 834.95 0.00
Al 4 4 0.22145E+08 45.00 0.95947E+00 0.40525E-01 0.00000E+00 0.00000E+00 0.15943E-01 -.94561E+07 0.10000E+01 834.49 0.00
Al 5 5 0.22106E+08 45.00 0.96055E+00 0.39446E-01 0.00000E+00 0.00000E+00 0.15936E-01 -.94561E+07 0.10000E+01 834.14 0.00
Al 6 6 0.22075E+08 45.00 0.96205E+00 0.37946E-01 0.00000E+00 0.00000E+00 0.15931E-01 -.94561E+07 0.10000E+01 833.86 0.00
Al 7 7 0.22048E+08 45.00 0.96166E+00 0.38340E-01 0.00000E+00 0.00000E+00 0.15927E-01 -.94561E+07 0.10000E+01 833.62 0.00
Al 8 8 0.22025E+08 45.00 0.96045E+00 0.39549E-01 0.00000E+00 0.00000E+00 0.15923E-01 -.94561E+07 0.10000E+01 833.41 0.00
Al 9 9 0.22005E+08 45.00 0.96181E+00 0.38190E-01 0.00000E+00 0.00000E+00 0.15920E-01 -.94561E+07 0.10000E+01 833.23 0.00
Al 10 10 0.21987E+08 45.00 0.96354E+00 0.36461E-01 0.00000E+00 0.00000E+00 0.15916E-01 -.94561E+07 0.10000E+01 833.06 0.00
Al 11 11 0.21970E+08 45.00 0.96205E+00 0.37947E-01 0.00000E+00 0.00000E+00 0.15913E-01 -.94561E+07 0.10000E+01 832.91 0.00
Al 12 12 0.21955E+08 45.00 0.96121E+00 0.38790E-01 0.00000E+00 0.00000E+00 0.15911E-01 -.94561E+07 0.10000E+01 832.77 0.00
Al 13 13 0.21941E+08 45.00 0.96235E+00 0.37652E-01 0.00000E+00 0.00000E+00 0.15908E-01 -.94561E+07 0.10000E+01 832.64 0.00
Al 14 14 0.21927E+08 45.00 0.96271E+00 0.37294E-01 0.00000E+00 0.00000E+00 0.15906E-01 -.94561E+07 0.10000E+01 832.52 0.00
Al 15 15 0.21915E+08 45.00 0.96180E+00 0.38201E-01 0.00000E+00 0.00000E+00 0.15904E-01 -.94561E+07 0.10000E+01 832.40 0.00
Al 16 16 0.21903E+08 45.00 0.96306E+00 0.36940E-01 0.00000E+00 0.00000E+00 0.15902E-01 -.94561E+07 0.10000E+01 832.30 0.00
Al 17 17 0.21892E+08 45.00 0.96448E+00 0.35525E-01 0.00000E+00 0.00000E+00 0.15900E-01 -.94561E+07 0.10000E+01 832.19 0.00
Al 18 18 0.21882E+08 45.00 0.96256E+00 0.37440E-01 0.00000E+00 0.00000E+00 0.15898E-01 -.94561E+07 0.10000E+01 832.10 0.00
Al 19 19 0.21872E+08 45.00 0.96256E+00 0.37438E-01 0.00000E+00 0.00000E+00 0.15897E-01 -.94561E+07 0.10000E+01 832.01 0.00
Al 20 20 0.21862E+08 45.00 0.96446E+00 0.35544E-01 0.00000E+00 0.00000E+00 0.15895E-01 -.94561E+07 0.10000E+01 831.92 0.00
```

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## Pressure and Saturation Profiles from Radial Flow Problem



Similarity variable:  $R^2/t$

Spatial profile at  $t = 8.64 \times 10^7$  s

Time series at  $R = 25.25$  m

Thin line: earlier LBNL results with “evaporation model”

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## Questions rcc3

- Modify rcc3, for example:
  - Make simulation non-isothermal
  - Add permeability reduction due to salt precipitation
  - Change thermodynamic models in *SELEC* block
  - Refine or coarsen mesh
  - Stop CO<sub>2</sub> injection; observe pressure recovery and phase redistribution
  - Change capillary pressure and relative permeability functions and observe impact in residual CO<sub>2</sub> trapping
- For each modification, discuss effect on simulation results

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